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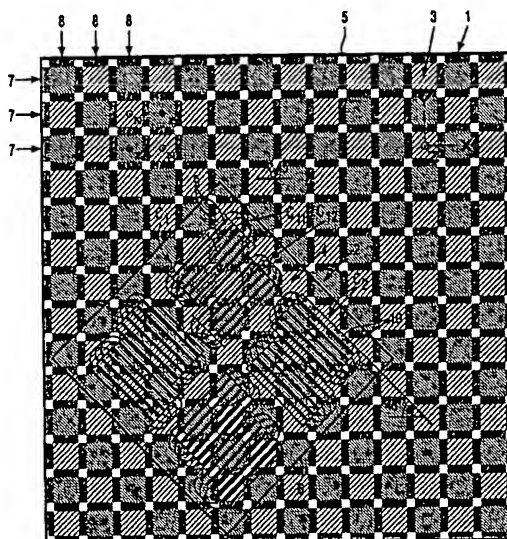
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(54) **Title: DISPLACEMENT DEVICE**



(57) **Abstract:** A positioning device comprising a first part (1) which is movable relatively to a second part (2) in an X-direction and a Y-direction, said first part (1) comprising a carrier (5) on which a system of magnets (3) is arranged according to a pattern of rows (7) and columns (8) extending parallel to the X-direction and the Y-direction, respectively. The magnets in each row and column are arranged according to a Halbach array, i.e. the magnetic orientation of successive magnets in each row (7) and each column (8) rotates 90° counter-clockwise. The second part (2) comprises an electric coil system (4) with two types of electric coils (C₁, C₂), one type having an angular offset of +45°, and the other type having an offset of -45° with respect to the X-direction. The magnet configuration causes a very strong magnetic field.

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Displacement device.

The invention relates to a displacement device comprising a first part and a second part which can be displaced with respect to each other in at least an X-direction and a Y-direction perpendicularly thereto, the first part comprising a carrier which extends substantially parallel to the X-direction and the Y-direction and on which a system of
5 magnets is secured in accordance with a pattern of rows extending parallel to the X-direction, and columns extending parallel to the Y-direction, an equal distance being present between the rows and between the columns, and magnets of a first type, having a magnetization direction which extends at right angles to the carrier and towards the second part, and magnets of a second type, having a magnetization direction which extends at right angles to
10 the carrier and away from the second part, being alternately arranged in each row and in each column, and a magnet of a third type being arranged in each column between each pair of juxtaposed magnets of the first and the second type, which magnet of a third type has a magnetization direction which extends parallel to the Y-direction and towards the magnet of the first type, while the second part is provided with an electric coil system comprising at
15 least one electric coil of a first type which has current conductors which are situated in a magnetic field of the system of magnets and which include an angle of substantially 45° with the X-direction, and comprising at least one electric coil of a second type, which has current conductors which are also situated in the magnetic field of the system of magnets and which include an angle of substantially 45° with the X-direction, and said current conductors
20 extending perpendicularly to the current conductors of the first electric coil.

Such a displacement device is disclosed in US 5,886,432 and can be used, inter alia, in a wafer stepper for manufacturing integrated circuits. The device enables very accurate and rapid displacements in the X and Y-directions to be made. In addition, small displacements in a Z-direction, perpendicularly to the X and Y-directions, are also possible.
25 The displacements depend upon the phase and the size of the current through the coils. In the system of magnets, a so-called Halbach magnet configuration is employed. In this configuration, the magnets of a series of magnets are magnetized such that the magnetization direction of each magnet of a pair of juxtaposed magnets is rotated through 90° with respect to the other magnet. The use of such a magnet configuration leads to a stronger magnetic

field on the side of the coils and hence to larger forces for displacing the parts with respect to each other. In US 5,886,432, a number of adjacent columns of magnets in accordance with the Halbach principle are used. The distance between the columns of magnets is equal to the width of a magnet. Consequently, there is air between the columns.

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It is an object of the invention to improve the displacement device in accordance with the first paragraph by optimizing the system of magnets.

To achieve this, the displacement device in accordance with the invention is characterized in that in each row of magnets of the first part, also a magnet of the third type is arranged between each pair of juxtaposed magnets of the first and the second type, which magnet of the third type has a magnetization direction extending parallel to the X-direction and towards the magnet of the first type.

Such a configuration of magnets leads to an even stronger magnetic field per unit of area surface, as compared to that obtained using the system of magnets in accordance with US 5,886,432, because, in accordance with the invention, also in the space between the columns magnets are arranged in accordance with a certain pattern, leading to a more efficient configuration of magnets and hence a stronger magnetic field. In fact, a Halbach configuration of magnets is now obtained both in the X-direction and in the Y-direction.

A further improvement of the displacement device is achieved in that the magnets of the first and the second type have an identical square shape with side faces, in that the magnets of the third type are rectangular in shape with side faces, whereby the longest side faces of a magnet of the third type border on the side faces of a magnet of the first and the second type and are just as long as the side faces of the magnet of the first and the second type, and the ratio of the dimension of the shortest side face of a magnet of the third type to the dimension of the longest side face ranging between 0.25 and 0.50. It has been found that this configuration of magnets yields an even stronger magnetic field.

When the parts are displaced with respect to each other by appropriately leading current through the coils, using commutation of the currents, i.e. a place-dependent current in a current conductor, it has been found that the movable part makes a slightly oscillating movement in the X-Y plane. Although the oscillation is only very small, it can be disturbing in applications for which the displacement device is intended, such as in a wafer stepper, but also in a component placement machine, wherein a high accuracy is required. This is caused by the fact that the distribution of the magnetic field over the current

conductor changes during the displacement of the coil, resulting in a variable torque exerted on the current conductor and hence on the second part.

These oscillating movements can be reduced in that the electric coil used in the displacement device in accordance with the invention comprises two sets of coils for each type, which are
5 each fed by an n-phase current system, wherein $n \geq 2$, and wherein, viewed in the longitudinal direction of the current conductors situated in the effective magnetic field, one set of coils is shifted with respect to the other set of coils over a distance approximately equal to half the pole pitch of the magnets, and wherein the pole pitch of the magnets is defined as
10 the distance between two adjacent diagonal lines on which center points of magnets of the same type, i.e. N and Z, are situated. An explanation for this is that the sum of the Lorentz forces in the coils yield only a minimum torque.

It is further advantageous if the length of the current conductors of the coils, which current conductors are situated in the effective magnetic field, is approximately equal to k times the pole pitch of the magnets, with k being 2, 4, 6, ..., and the pole pitch of the
15 magnets being defined as the distance between two adjacent diagonal lines on which center points of magnets of the same type are situated. A movement in the longitudinal direction of the current conductors causes the sum of the magnetic field to remain substantially constant, as a result of which fluctuations in the strength are reduced.

These and other aspects of the invention will be apparent from and elucidated
20 with reference to the embodiments described hereinafter.

In the drawings:

Fig. 1 is a diagrammatic plan view of the displacement device comprising the
25 system of magnets and the electric coil system,

Fig. 2 is a detailed plan view of Fig. 1,

Fig. 3 is a cross-sectional view of the displacement device shown in Fig. 1,

Fig. 4 shows an example of the application of the displacement device of Fig.
1 in a component placement machine, and

30 Fig. 5 shows an example of the application of the displacement device shown in Fig. 1 in a wafer stepper for the lithographic manufacture of integrated circuits.

Fig. 1 diagrammatically shows a displacement device comprising a first part 1 formed by a system 3 of magnets, and a second part 2 formed by an electric coil system 4. The magnets are secured onto a carrier 5 and the coil system is secured onto a coil block 6. The first and the second part can move with respect to each other. In general, the stationary part is formed by the carrier 5 with the magnets, and the movable part is formed by the coil block 6.

The magnets are arranged on the carrier 5 in the manner described hereinafter: the magnets are arranged in a pattern of rows 7 extending parallel to the X-direction, and columns 8 extending parallel to the Y-direction, the interspace between the rows and between the columns being the same. In each row 7 and in each column 8, magnets of a first type N and of a second type Z are alternately arranged. The magnets of the first type N have a direction of magnetization which extends at right angles to the carrier and towards the second part with the electric coil system, while the magnets of the second type Z have a direction of magnetization which extends at right angles to the carrier and away from the second part with the electric coil system. In each row and in each column, a magnet of a third type H is arranged between each pair of magnets of the first type N and the second type Z. The direction of magnetization of the magnets of the third type H which are situated between the columns 8, extends parallel to the Y-direction and towards the adjacent magnet of the first type N, while the direction of magnetization of the magnets of the third type H which are situated between the rows 7, extends parallel to the X-direction and also towards the adjacent magnet of the first type N. The directions of magnetization of the different types of magnets N, Z and H are indicated by means of arrows.

The electric coil system 4 is provided with at least one coil of a first type C_1 whose current conductors 9, which are situated in the effective magnetic field of the magnets, include an angle of 45° with the X-direction, and said electric coil system is also provided with at least one coil of a second type C_2 having current conductors 10, which are also situated in the effective magnetic field of the magnets, include an angle of 45° with the X-direction, and extend perpendicularly to the current conductors 9 of the coil of the first type C_1 . The expression "current conductors in the effective magnetic field", is to be taken to mean that that part of the coil, generally a bunch of current conductors, is situated in the magnetic field of the magnets, and that an effective Lorentz force is exerted on said part, causing a movement of the coil.

The manner in which the coils move in the system of magnets will be explained hereinafter with reference to Fig. 2. The reference numerals 9_1 , 9_2 and 10_1 , 10_2

represent current conductors of the coils C_1 and C_2 , respectively, which are provided in the magnetic fields of the magnets. Current conductor 9_1 is situated predominantly in the magnetic fields of the magnets indicated by means of the letter N. The direction of magnetization of these N magnets is indicated by means of an arrow pointing upwards, i.e. directed at right angles to the system of magnets and towards the current conductor 9_1 . The direction of the magnetic field is indicated by means of the arrow B_1 . If an electric current flows through the current conductor 9_1 in the direction indicated by the arrow I_1 , a force F_1 will be exerted on the current conductor in the direction indicated by the relevant arrow, as a result of which the current conductor wants to start moving in the direction of the arrow F_1 .

Current conductor 9_2 is predominantly situated in the magnetic fields of the magnets referenced Z. The direction of magnetization of these Z magnets is indicated by means of an arrow B_2 which points downwards, i.e. at right angles to the system of magnets and away from the current conductor 9_2 . If an electric current flows through the current conductor 9_2 in accordance with the arrow I_2 , i.e. it runs counter to the current I_1 , a force F_2 in the direction indicated by the relevant arrow will be exerted on the current conductor 9_2 , as a result of which the current conductor wants to start moving in the direction indicated by the arrow F_2 , i.e. in the same direction as the arrow F_1 . In the same manner, the current conductors 10_1 and 10_2 , which are arranged at right angles to the current conductors 9_1 and 9_2 , will be subject to a force extending in the direction indicated by the arrows F_3 and F_4 , under the influence of the magnetic fields of the N and Z magnets at a current in accordance with the arrows I_3 and I_4 . Of course, if the currents in the current conductors are reversed, the force exerted on, and hence the movement of the current conductors, will also be reversed. In Fig. 3, this interplay of forces is also shown.

Parts 11 of current conductors 9, 10 are also present above the magnets of the third type H and/or above parts where there is no magnet, i.e. between the magnets of the first type N and the second type Z (see Fig. 2, bottom left). These parts of the current conductors are situated in a magnetic field B whose average direction extends substantially parallel to the X-Y plane. Reference is also made to current conductor 9_{1c} in Fig. 3. If a current I runs through this current conductor, the above-mentioned parts of the current conductor will be subject to a force F in a direction perpendicular to the X-Y plane, i.e. the Z-direction. Dependent upon the direction of the current and the position of the current conductor with respect to the magnets, the force will be directed towards the magnets or away from the magnets. If the force is directed away from the magnets, then this force is referred to as the

levitation force F_1 , i.e. a force causing the current conductor to move away from the magnets. Such a force can be used to provide bearing between the coil block and the magnets.

The magnets of the first type N and the second type Z are square in shape. The magnets of the third type H are rectangular and dimensioned so that (see Fig. 2) the longest side faces 12 of a H magnet border on the side faces 13 of an N magnet and a Z magnet, and the ratio between the dimension of the shortest side face 14 and the dimension of the longest side face 12 of a H magnet lies in the range between 0.25 and 0.50. This results, as has been found in an optimization analysis, in the greatest strength of the magnetic field per unit area of the magnet system.

Fig. 3 shows two sets of three coils, i.e. a first set C_{11} with current conductors 9_{1a} , 9_{1b} , 9_{1c} and return current conductors 9_{2a} , 9_{2b} , 9_{2c} , and a second set C_{21} with current conductors 9_{3a} , 9_{3b} , 9_{3c} and return current conductors 9_{4a} , 9_{4b} , 9_{4c} . Both sets of coils are fed by a three-phase current system. Viewed in the longitudinal direction of the current conductors, the first set C_{11} of three current conductors is shifted over a distance 15, which is approximately half the pole pitch 16 of the magnets, with respect to the second set C_{21} of three current conductors. The pole pitch 16 of the magnets is to be taken to mean herein the distance between two adjacent diagonal lines on which the center points 17 and 18 of magnets of the same type, respectively, N and Z are situated. If this measure is not taken, a variable torque is exerted on both sets of current-carrying coils during the displacement, which torque causes a kind of oscillating movement of the moving part (coil block or carrier with magnets) around the Z-axis with respect to the stationary part. By virtue of the displacement of the sets of coils with respect to each other, this oscillating effect is substantially reduced because a torque develops in one of the two sets of coils, which compensates for the torque in the other set.

The length 19 of the current conductors is chosen to be such that it is approximately equal to k times the pole pitch 16 of the magnets, k being a multiple of 2. As a result, upon a movement of the current conductor in the longitudinal direction the sum of the magnetic field remains approximately constant. This causes fluctuations in the force exerted on the current conductor to be smaller. This application is not dependent on the coils and phases.

Fig. 4 shows an example of an application of the displacement device in a component placement machine. The stationary part 1 is formed by a carrier 5 on which the

system 3 of magnets is arranged, and which is rigidly attached to a machine frame 20. The magnets are downwardly directed, in the direction of a printed circuit board 21 on which components 22 must be placed. Just below the magnets there is the movable part 2 with the coil block 6 on which the coil system 4 is provided. A placement head 23 is attached to the
5 movable part 2. The placement head is provided, for example, with a gripping element or a suction pipette 24 by means of which components can be picked up from a feeder (not shown), whereafter they are placed on the printed circuit board. The placement head may be additionally provided with a separate motor 25 for making a movement in the Z-direction and a rotation about the Z-axis (ϕ movement). If the current is properly commuted, the placement
10 head can reach any desired position in the X-Y plane and, thus, place a component in the desired position on the printed circuit board. An iron plate 26 is also attached to the coil block 6, as a result of which the coil block 6 is subject to a force in the direction of the magnets. When a current flows through the coils, the levitation force is such that it compensates for the attractive force exerted by the magnets on the iron plate and hence on the
15 coil block. Consequently, when no current flows through the coils, there is no levitation force and the coil block is pulled against the magnets, so that the placement head is automatically attached. As a result, separate bearing and attachment of the placement head is not necessary.

Fig. 5 shows an example of an application of the displacement device in a wafer stepper for the lithographic manufacture of integrated circuits. The wafer stepper
20 comprises a frame 30 for supporting a displacement device 31, a focusing unit 32, a mask holder 33 and a radiation source 34. The radiation source 34 is provided with a light source 35. On the mask holder 33 a mask 36 can be placed, which is provided with a pattern of an integrated semiconductor circuit. The focusing unit is an image or projection system provided with an optical lens system 37 with an optical axis 38. An identification unit 39 is also
25 attached to the frame 30. The displacement device 31 comprises the carrier 5 on which the system of magnets 4 is provided. The carrier 5 is attached to the frame 30. The displacement device further comprises a first and a second coil block 6a and 6b, respectively, which each have a substrate holder 40 and 41, respectively, on which semiconductor substrates 42 and 43, respectively, can be placed. The coil blocks with the substrate holders can be
30 independently sent to any position in the X-Y plane above the system of magnets. This has the advantage that operations, such as moving the substrate holders from and to a load and unload position (not shown), an identification position (below the identification unit 39) and an illumination position (below the focusing unit 32) can be carried out simultaneously and completely independently, so that a larger output is obtained. Also in this construction, the

levitation force enables the substrate holder to be bearing-supported with respect to the magnet surface.

CLAIMS:

1. A displacement device comprising a first part (1) and a second part (2) which can be displaced with respect to each other in at least an X-direction and a Y-direction perpendicularly thereto, the first part comprising a carrier (5) which extends substantially parallel to the X-direction and the Y-direction and on which a system (3) of magnets is secured in accordance with a pattern of rows (7) extending parallel to the X-direction, and columns (8) extending parallel to the Y-direction, an equal distance being present between the rows and between the columns, and magnets of a first type (N), having a magnetization direction which extends at right angles to the carrier (5) and towards the second part (2), and magnets of a second type (Z), having a magnetization direction which extends at right angles to the carrier (5) and away from the second part (2), being alternately arranged in each row (7) and in each column (8), and a magnet of a third type (H) being arranged in each column (8) between each pair of juxtaposed magnets of the first (N) and the second type (Z), which magnet of a third type has a magnetization direction which extends parallel to the Y-direction and towards the magnet of the first type (N), while the second part (2) is provided with an electric coil system (4) comprising at least one electric coil of a first type (C₁) which has current conductors (9) which are situated in a magnetic field of the system of magnets and which include an angle of substantially 45° with the X-direction, and comprising at least one electric coil of a second type (C₂), which has current conductors (10) which are also situated in the magnetic field of the system of magnets and which include an angle of substantially 45° with the X-direction, and said current conductors extending perpendicularly to the current conductors (9) of the first electric coil (C₁), characterized in that in each row (7) of magnets of the first part (1), also a magnet of the third type (H) is arranged between each pair of juxtaposed magnets of the first (N) and the second type (Z), which magnet of the third type has a magnetization direction extending parallel to the X-direction and towards the magnet of the first type (N).

2. A displacement device as claimed in claim 1, characterized in that the magnets of the first (N) and the second (Z) type have an identical square shape with side faces (13), in that the magnets of the third type (H) are rectangular in shape with side faces (12, 14),

whereby the longest side faces (12) of a magnet of the third type (H) border on the side faces (13) of a magnet of the first (N) and the second (Z) type and are just as long as the side faces (13) of the magnet of the first and the second type, and the ratio of the dimension of the shortest side face (14) of a magnet of the third type (H) to the dimension of the longest side face (12) ranging between 0.25 and 0.50.

3. A displacement device as claimed in claim 1 or 2, characterized in that each electric coil (C_1 , C_2) comprises two sets (C_{11} , C_{12}) of coils which are each fed by an n-phase current system, wherein $n \geq 2$, and wherein, viewed in the longitudinal direction of the current conductors (9_{1a} - 9_{4c}) situated in the effective magnet field, one set (C_{11}) of coils is shifted with respect to the other set (C_{12}) of coils over a distance approximately equal to half the pole pitch of the magnets, and wherein the pole pitch of the magnets is defined as the distance between two adjacent diagonal lines on which center points (17) and (18), respectively, of magnets of the same type (N) and (Z) are situated.

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4. A displacement device as claimed in any one of the preceding claims, characterized in that the length (19) of the current conductors (9, 10) of the coils, which current conductors are situated in the effective magnetic field, is approximately equal to k times the pole pitch (16) of the magnets, with k being 2, 4, 6, ..., and the pole pitch (16) of the magnets being defined as the distance between two adjacent diagonal lines on which center points (17) and (18), respectively, of magnets of the same type (N) and (Z) are situated.

20

5. Component placement machine comprising a machine frame (20) and a placement head (23) for placing components (22) on a printed circuit board (21), which placement head can be displaced by means of a displacement device as claimed in any one of the claims 1-4, wherein the stationary part (1) of the displacement device is secured to the machine frame (20), while the placement head (23) is secured to the movable part (2) of the displacement device.

25

6. A lithographic device for the manufacture of integrated circuits on a semiconductor substrate (42, 43), comprising a frame (30), a radiation source (34), a mask holder (33) and a substrate holder (40, 41), which mask holder can be displaced by means of a displacement device as claimed in any one of the claims 1-4, wherein the carrier (5) of the

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stationary part of the displacement device is secured to the frame (30), while the substrate holder (40, 41) is secured to the movable part with the coil blocks (6a, 6b).

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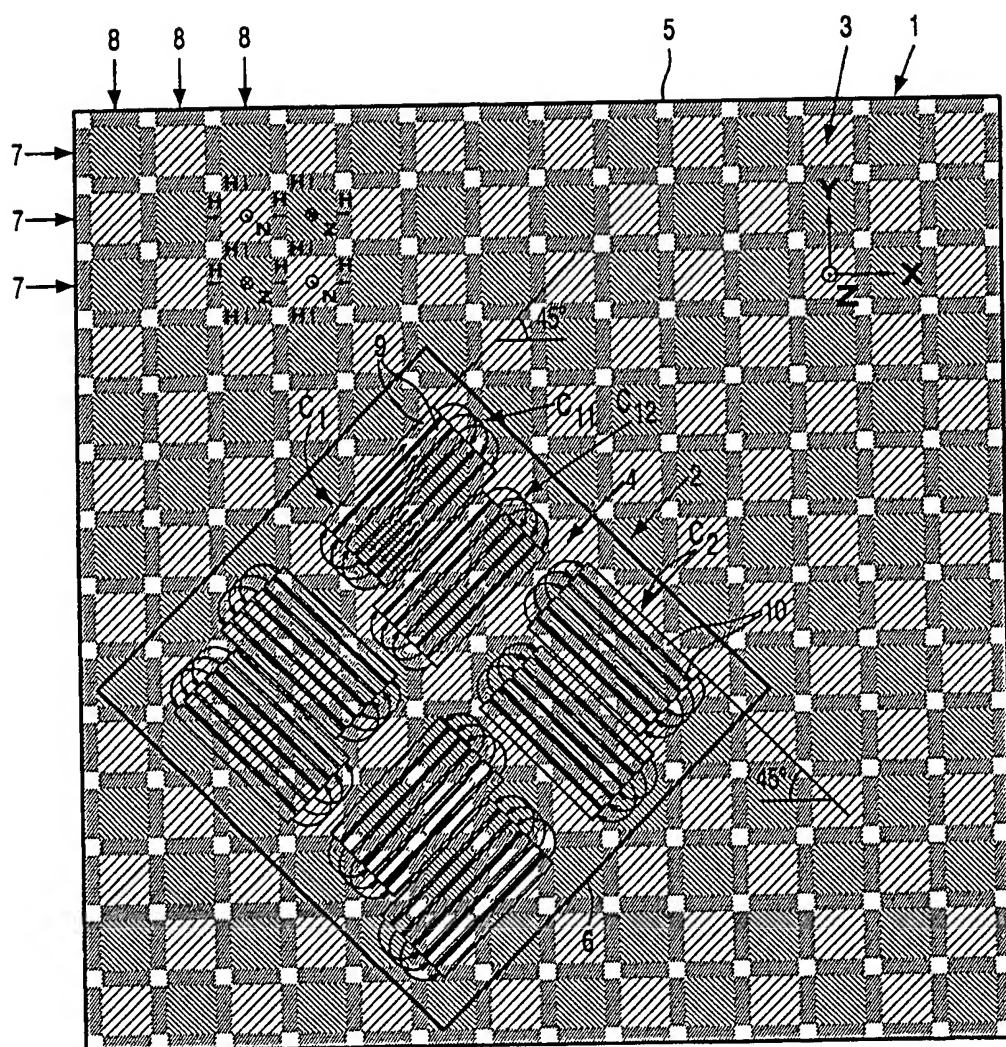


FIG. 1

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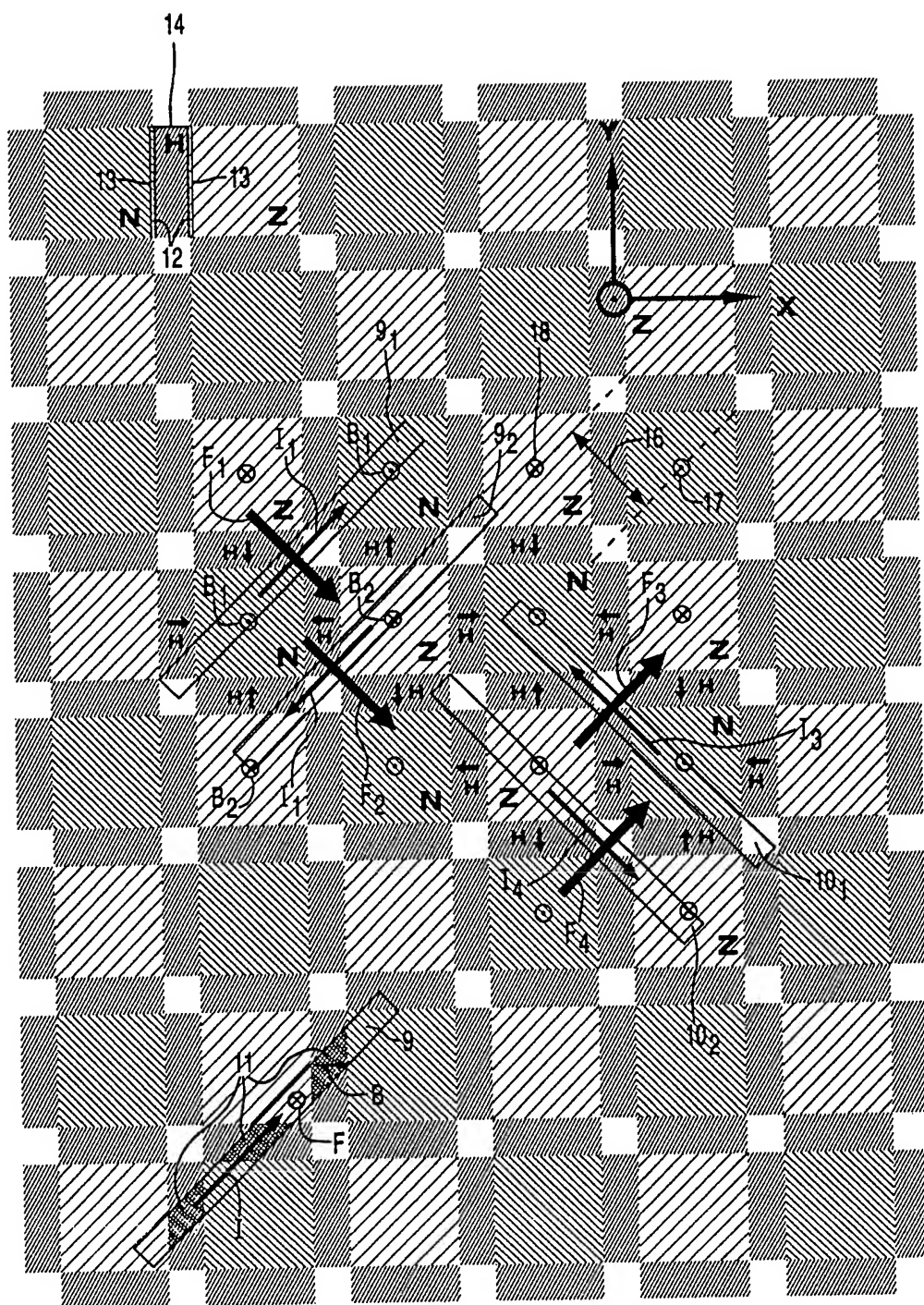


FIG. 2

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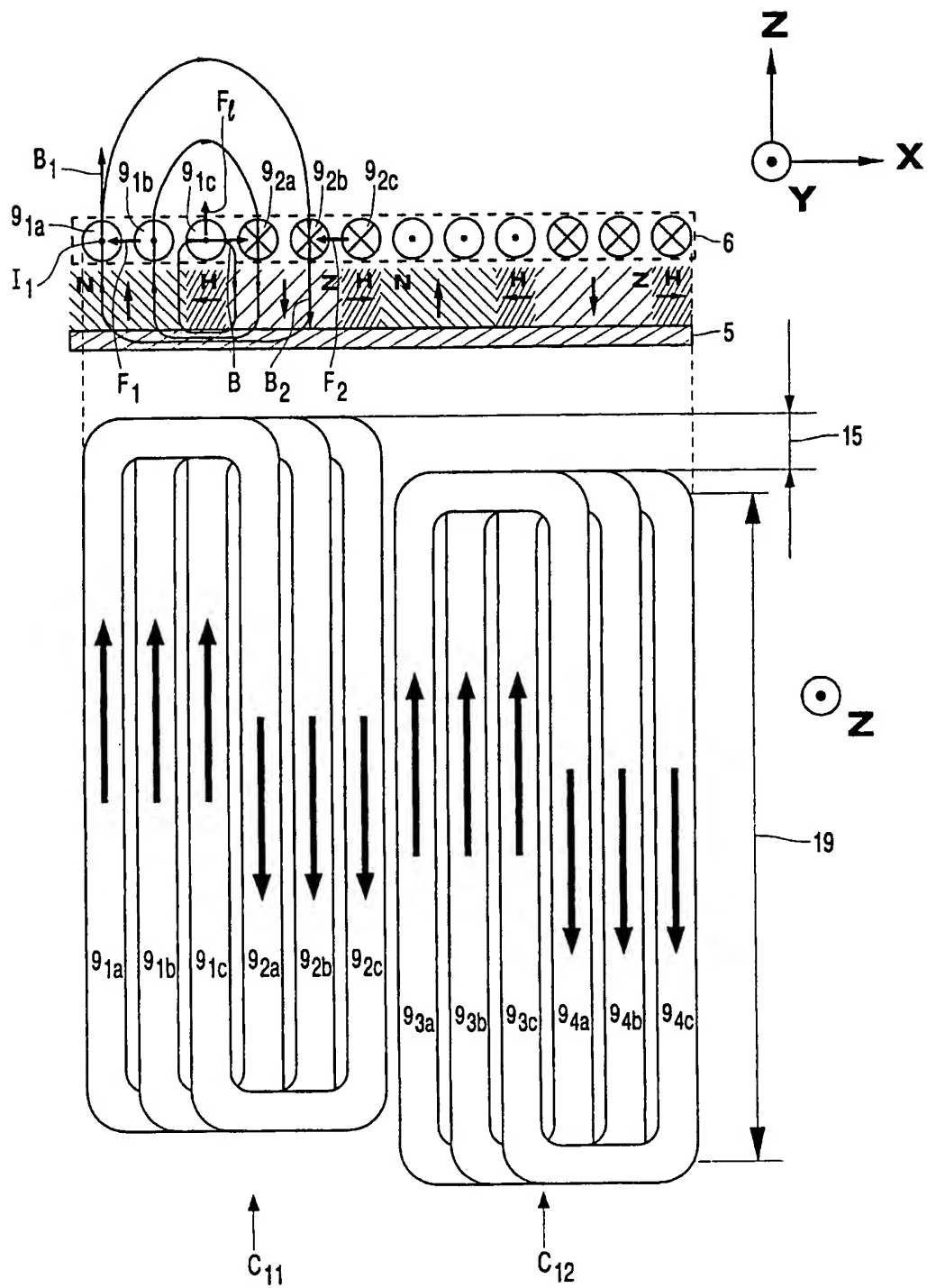


FIG. 3

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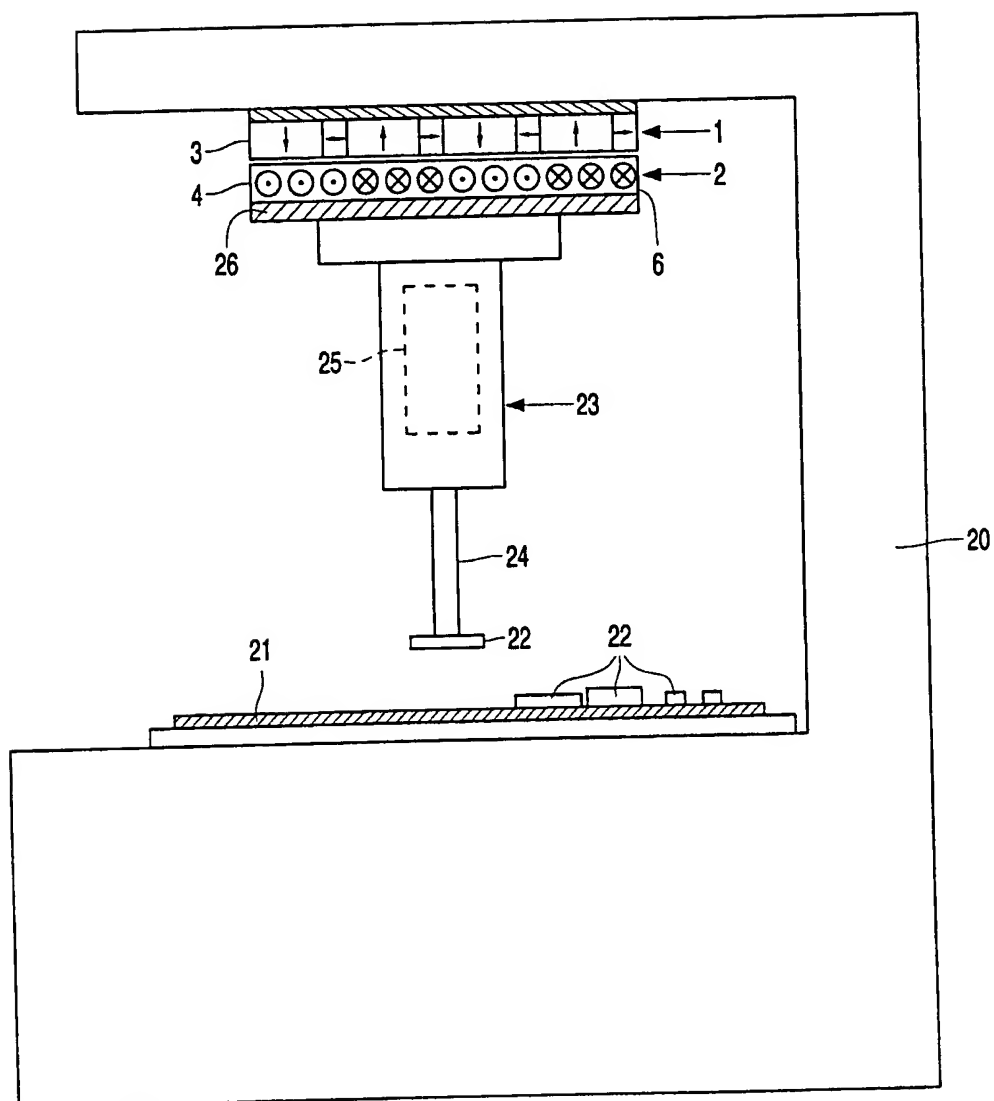


FIG. 4

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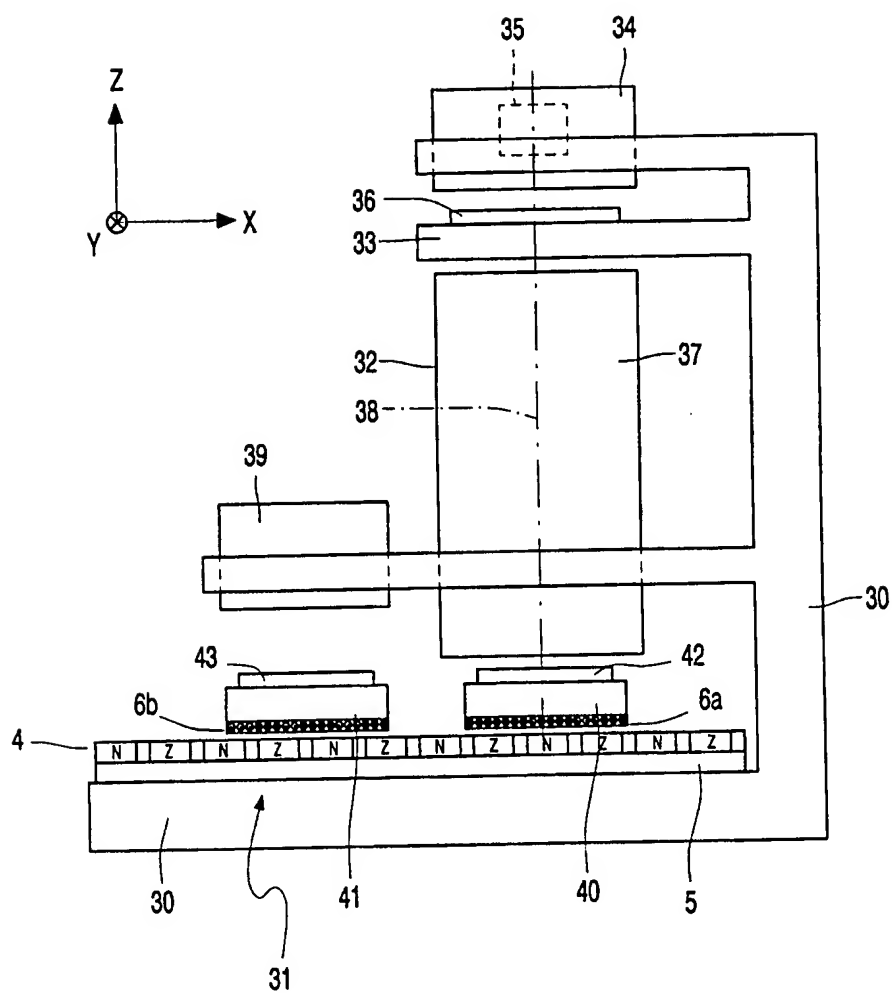


FIG. 5

INTERNATIONAL SEARCH REPORT

International Application No
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A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 H02K41/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 H02K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)
EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 99 04481 A (TANAKA KEIICHI ;NIPPON KOGAKU KK (JP)) 28 January 1999 (1999-01-28) figures 3,5	1
X,P	US 6 072 251 A (MARKLE DAVID A) 6 June 2000 (2000-06-06) figures	1
A	US 5 886 432 A (MARKLE DAVID A) 23 March 1999 (1999-03-23) cited in the application	

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☒ Patent family members are listed in annex.

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INTERNATIONAL SEARCH REPORT

Information on patent family members

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